

DETERMINATION OF STRESSES IN THE STEEL PIPE DURING THE SUPERFICIAL HEAT TREATMENT PROCESS WITH HELICAL PATH

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Abstract. In the paper a numerical model for the quench hardening process with the moving heat source of steel pipe made of medium carbon steel have been presented. The constant speed rotation and moving of the pipe was assumed to obtain the path of the heat source in the shape of the helical line. In this model the relationship occurring between thermal phenomena, phase transformation in the solid state and mechanical phenomena have been taken into account. The temperature and stress fields are determined using the copyright software based on the finite element method (three-dimensional tasks). To calculate the phase content in the solid state, the macroscopic model based on the analysis of the CTP diagrams is used. The range of the martensite transformations depends on the value of stresses. In the model the tempering phenomena is also taken into account. In the model of mechanical phenomena the elastic, thermal, structural, plastic strains and transformations plasticity are considered.

Keywords: *numerical analysis, superficial heat treatment, phase transformations in the solid state, stresses, steel pipe*

1. Introduction

The optimization of production costs of the machine parts at the design stage requires proper selection of material properties, not always the same in the entire area of the workpiece. In the production of machine parts the more cheaper materials are used. In the load area the material properties are improved by using the treatment processes. Therefore, the simulation tools for optimization of industrial processes are used.

One of the basic process, which aims to improve the mechanical properties of the steel part, is quench hardening. In some processes, in which previously the volumetric hardening has been used, often the heat treatment with the moving heat source is applied. The use of this technology allows for more precise control of material parameters and reduces the energy intensity of the process.

2. Numerical model

For modelling of the quench hardening process the complex numerical model taking into account thermal phenomena, phase transformations in the solid state and mechanical phenomena are used. Coupling between elements of the model (see Fig. 1) such as: latent heat of phase transformations (unimportant phenomena during the superficial hardening process), structural and thermal strains as well as transformation plasticity should also be taken into consideration. The influence of temperature and phase composition on the properties of hardened material (heat transfer coefficient, thermal capacity, Young's modulus and yield point for the appropriate phase) and influence of the stress state on the range of phase transformations should also be presented on this model.

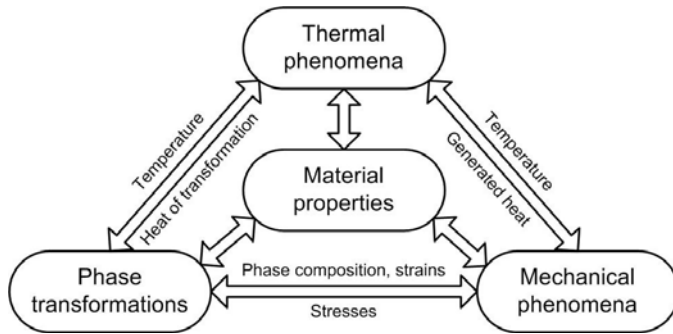


Fig. 1. The diagram of numerical model for quench hardening process

To determine the temperature fields, in the next time steps, the solution of the heat transfer equation based on the finite element method is used

$$\nabla \cdot (\lambda \nabla T) - \rho C \frac{\partial T}{\partial t} = 0 \quad (1)$$

where: T is temperature [K], t is time [s], $\lambda = \lambda(T)$ is the thermal conductivity [W/(m·K)], ρ is the density [kg/m³], C is the effective thermal capacity [J/(kg·K)].

The superficial heat source (Neumann boundary condition) in the simulation of the heating process is determined by the function

$$q(s, z) = \frac{Q}{2\pi R^2} \exp\left(-\frac{(s_z - s_z^0)^2 + (z - z_0)^2}{2R^2}\right) \quad (2)$$

where: Q is the power of the source [W], R is the radius of the source, $s_z^0 = P(x_0(\varphi), y_0(\varphi))$, $s_z = r_z(\varphi)$, φ the angle of the position of the source, r_z is the external radius.

To calculate the kinetic of phase transformations in the solid state during the heating and cooling processes, the macroscopic model based on the analysis of CTP diagrams is used.

The fraction of the austenite phase during heating is determined on the basis of modified Koistinen-Marburger equation [1]

$$\tilde{\eta}_{\gamma}(T, t) = 1 - \exp\left(-\frac{4.60517}{T_{s\gamma} - T_{f\gamma}}(T_{s\gamma} - T)\right) \quad (3)$$

The phase transformations during the cooling process are calculated by the Johnson-Mehl-Avrami-Kolmogorov equation

$$\eta_{(i)}(T, t) = \min\left\{\eta_{(i\%)}, \tilde{\eta}_{\gamma} - \sum_{j \neq i} \eta_j\right\} \cdot \left(1 - \exp\left(-\frac{0.01005}{t_s^{n(T)}} t^{n(T)}\right)\right) \quad (4)$$

where: $\eta_{(i\%)}$ is the final fraction of “i” phase estimation on the basis of CCT diagrams for considered steel, $n(T)$ the functions depending on the start and finish times of transformation (t_s and t_f), $T_{s\gamma}$ and $T_{f\gamma}$ are the temperature of start and finish of austenite transformation.

Increment of martensite phase is described by the Koistinen-Marburger equation [1, 2]

$$\eta_M(T, t) = \left(\tilde{\eta}_{\gamma} - \sum_{i \neq M} \eta_i\right) \left(1 - \exp(-0.0153(M_S - T + A_M(\sigma_{ii})/3 + B_M \sigma_{eff}))\right) \quad (5)$$

where: σ_{eff} is effective stress, M_S is the start temperature of martensite transformation, A_M and B_M are material coefficients.

The martensite tempered fraction resulting from tempering is described by formula

$$\eta_{(i)}(T, t) = \eta_M \left(1 - \exp\left(-\frac{0.01005}{t_s^{n(T)}} t^{n(T)}\right)\right) \quad (6)$$

The curves of start and finish of the tempering transformations were determined on the basis of equations dependent on the heating speed [3].

The thermal and structural strains are calculated by the following equations

$$\Delta \varepsilon^{TPh} = \Delta \varepsilon^T + \Delta \varepsilon^{Ph}, \quad \Delta \varepsilon^T = \sum_i \alpha_i(T) \eta_i \Delta T, \quad \Delta \varepsilon^{Ph} = \text{sign}(-\Delta T) \sum_i \varepsilon_i^{Ph}(T) \Delta \eta \quad (7)$$

where: $\alpha_i(T)$ is a thermal expansion coefficients for “i” phase, $\varepsilon_i^{Ph}(T)$ is a strain expansion coefficient for “i” transformation.

In the model of mechanical phenomena the equilibrium equation was used without mass forces. The equilibrium equations are supplemented by the constitutive relations in the form

$$\Delta \sigma = \mathbf{D} \circ \Delta \varepsilon^e + \Delta \mathbf{D} \circ \varepsilon^e, \Delta \varepsilon^e = \Delta \varepsilon - \Delta \varepsilon^T - \Delta \varepsilon^{ph} - \Delta \varepsilon^{pl} - \Delta \varepsilon^{tp} \quad (8)$$

where: ε^e , ε , ε^{pl} , ε^{tp} are respectively the elastic, total, plastic and transformation strain tensors, \mathbf{D} is tensor of material constants.

The plastic strains (ε^{pl}) are determined by using the associated plastic flow law with isotropic hardening [4]. To calculate transformations plasticity (ε^{tp}) the model based on the Greenwood-Johnson mechanism is used [4, 5]. The temporary yield point is dependent on the temperature and the phase composition.

3. Numerical simulation

The numerical simulation of the quench hardening process was performed for the pipe made of C45 steel. It was assumed that the considered object is only a part of a larger steel element which was assumed by appropriate conditions on the edge Γ_B . The dimensions of the medium carbon steel pipe are following: the length of the element 0.05 m, internal radius $r_w = 0.0225$ m and external radius $r_z = 0.025$ m (Fig. 2).

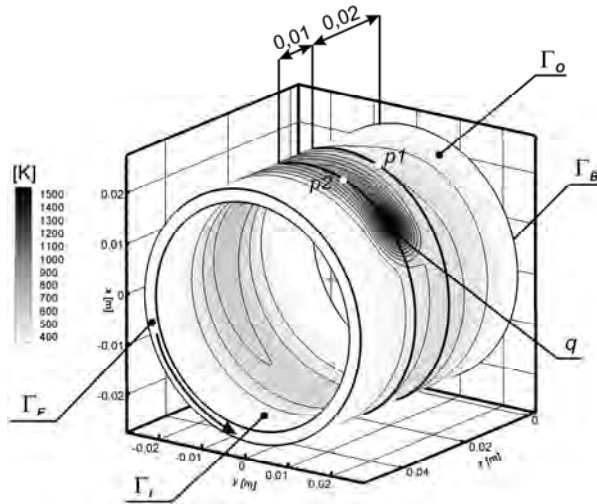


Fig. 2. Graphical interpretation of the described example

The following conditions to modelling of the quench hardening process were assumed:

- the initial temperature (T_0) in the whole area is equal to 293 K,
- the thermophysical properties such as: heat transfer coefficient, thermal capacity, Young's modulus and yield point for the appropriate phase depends on the temperature and phase composition [6],

- the parameters of the heat source: position $z = 0.02$ m, superficial heat source $R = 0.0033$ m, $Q = 1800$ W, hardening speed $V_\phi = 0.02$ m/s (0.8 rad/s),
- on boundaries Γ_F , Γ_O , Γ_I the Newton boundary condition (cooling in the air) with $T_{air} = 293$ K, (α_{air}) [7],
- on boundary Γ_B the Dirichlet boundary conditions $U_x = U_y = U_z = 0$, $T = 293$ K.

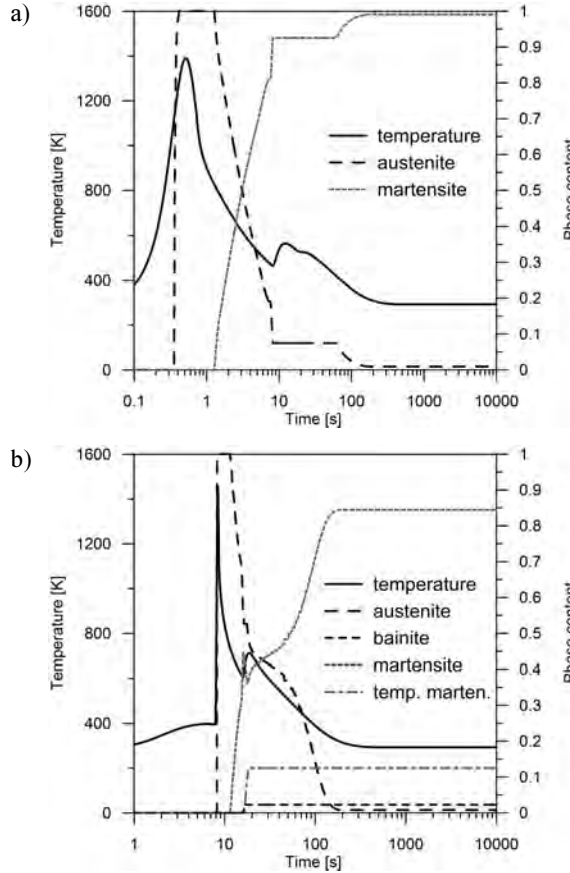
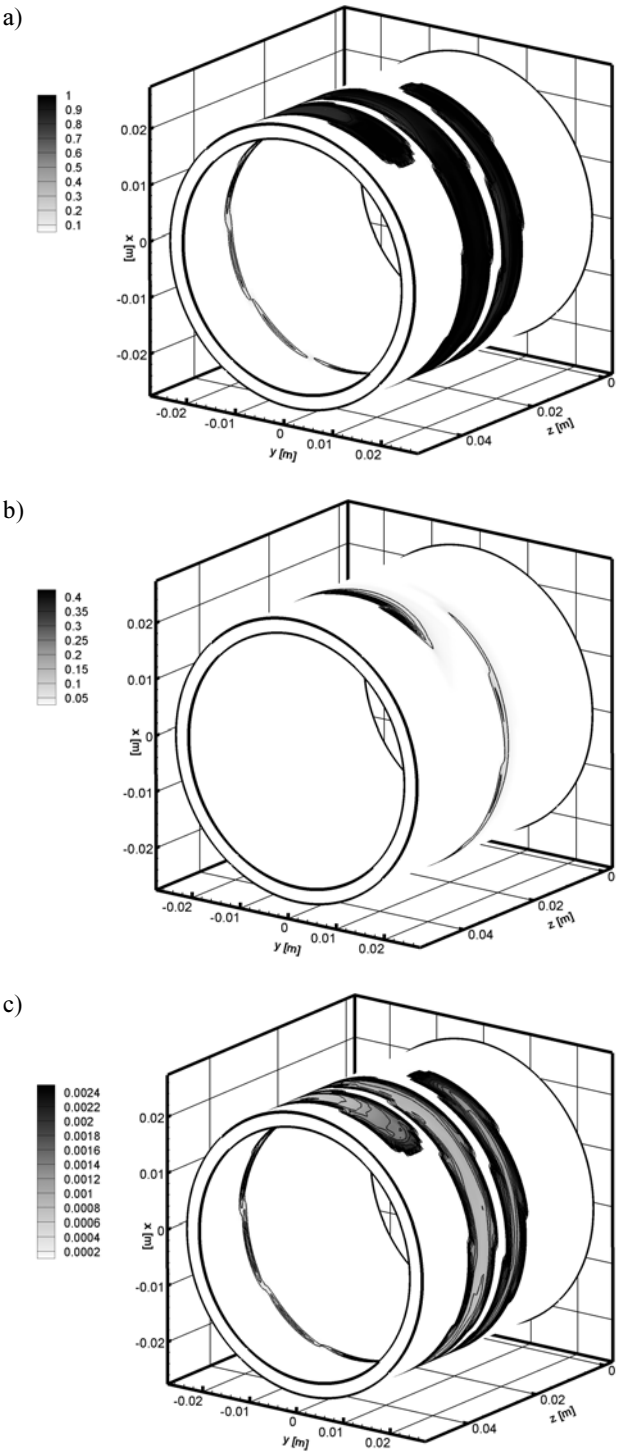


Fig. 3. Changes of temperature and phase fractions (austenite, bainite, martensite, tempered martensite) in control nodes: a) first control node, b) second control node

Results of numerical calculations showing the kinetic of phase transformations, distribution of temperature in two control nodes: p1(0.0077, 0.0238, 0.0204) and p2(0.0077, 0.0238, 0.0316) are depicted in Figures 2 and 3.

The path of the heat source in the shape of the helical line caused the influence of temperature on the next waveforms to be greater with the increasing of the temperature of element. Due to the gradual heating of the element the width of the heat affected zone is increasing. On the next paths the particular importance has the tempering process. Because of the shape of the path, the tempering process takes place only in the areas between the paths.



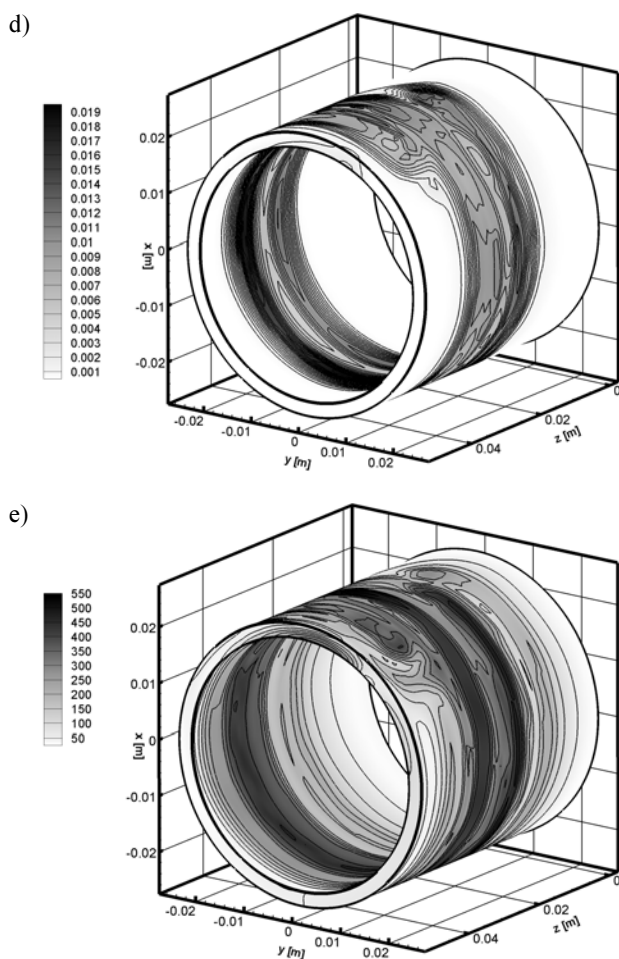


Fig. 4. Distributions of: a) martensite fraction, b) tempered martensite fraction, c) structural strains, d) residual effective plastic strain, e) residual effective stresses [MPa]

4. Conclusions

The characteristics of the results occurring in such simple technological process indicates on the very complex stress state. The use of heat source with constant power caused the increase of the martensite phase range in the following wave-forms. The changes of heat source power should be used to obtain uniform zones of martensite. Due to the use of a helical line of the heat source, the stress state is much more uniform than in the case of using circular paths (see Fig. 4) [8]. All calculations were performed on the copyrighted software implemented in C++ language.

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